

THE INFLUENCES OF ION IMPLANTATION DOSES TO COMMERCIALY PURE TITANIUM SURFACE HARDNESS

Agung Setyo Darmawan¹, Waluyo Adi Siswanto², Bambang Waluyo Febrianto¹,
and Tjipto Sujitno³

¹Jurusan Teknik Mesin, Universitas Muhammadiyah Surakarta (UMS),
Pabelan, Surakarta 57102, Indonesia.

²Department of Engineering Mechanics, Universiti Tun Hussein Onn Malaysia,
86400 Parit Raja, Batu Pahat, Johor, Malaysia

³National Nuclear Energy Agency (BATAN), Yogyakarta 55281, Indonesia
Email: agungsetyod@gmail.com

Abstract.

Commercially pure (cp) titanium has a relative soft hardness property. In particular usage such as sliding, the improvement of the hardness value will be required. To improve the hardness of the surface while maintaining the original properties, ion implantation process is conducted. Nitrogen ions are used to implant this material. The effects of the nitrogen ion doses to the surface hardness are then studied. In this study, Ion Implantation processes are conducted at room temperature and process durations are varied as 140 minutes, 280 minutes and 560 minutes. The doses of nitrogen ions which is required in these process durations are 8.4×10^{14} ions/cm², 16.8×10^{14} ions/cm², and 33.6×10^{14} ions/cm² respectively. Hardness tests are then performed on each specimen by using Micro Vickers Hardness Tester. The processes of ion implantation produce the hardness surface values of 88.97 HV, 125.51 HV, and 130.2 HV, for the doses of 8.4×10^{14} ions/cm², 16.8×10^{14} ions/cm², and 33.6×10^{14} ions/cm². The ion implantation of cp titanium can significantly increase the hardness on the surface. Compared to the hardness of the raw material, these processes have increased the hardness values by 64.8 %, 132.5 %, and 141.2 % for the doses of 8.4×10^{14} ions/cm², 16.8×10^{14} ions/cm², and 33.6×10^{14} ions/cm² respectively. The hardness can be improved as high as 41.07 % when the dose is increased from 8.4×10^{14} ions/cm² to 16.8×10^{14} ions/cm². However there is no a significant increasing in hardness value when the dose is increased from 16.8×10^{14} ions/cm² to 33.6×10^{14} ions/cm².

Keywords: *diffusion; hardness; implant material; surface hardening; vickers*

Introduction

Ion implantation is a special case of particle radiation. The process involves the bombardment of a solid material with medium to high energy ionized atoms into the near surface region of any substrate. This near surface alloying can be performed irrespective of thermodynamic criteria such as solubility and diffusivity. These advantages, coupled with the additional possibility of low-temperature processing, have prompted explorations into applications in which the limitations of dimensional changes and possible delaminating of conventional coatings are a concern (Hirvonen and Sartwell, 1994). Component dimensions or bulk material properties are not adversely affected by the process.

A schematic view of the path of an individual ion in ion implantation is shown in Figure 1. The individual ion loses its energy and creates a shallow surface-modified region. As illustrated in the figure, the ion does not travel in a straight path to its resting place, due to collisions with the target atoms. Target atoms are displaced from their lattice sites with sufficient energy that they can themselves displace additional target atoms, resulting in a collision cascade.

Ion implantation equipment typically consists of an ion source, where ions of the desired element are produced, an accelerator, where the ions are electrostatically accelerated to a high energy, and a target chamber, where the ions impinge on a target, which is the material to be implanted. The schematic of equipment setup and photograph of the device arrangement for plasma nitrocarburizing can be seen in Figure 2 and Figure 3, respectively.

Each ion is typically a single atom or molecule, and thus the actual amount of material implanted in the target is the integral over time of the ion current. This amount is called the dose. The currents supplied by implanters are typically small (microamperes), and thus the dose which can be implanted in a reasonable amount of time is small. Therefore, ion implantation finds application in cases where the amount of chemical change required is small.

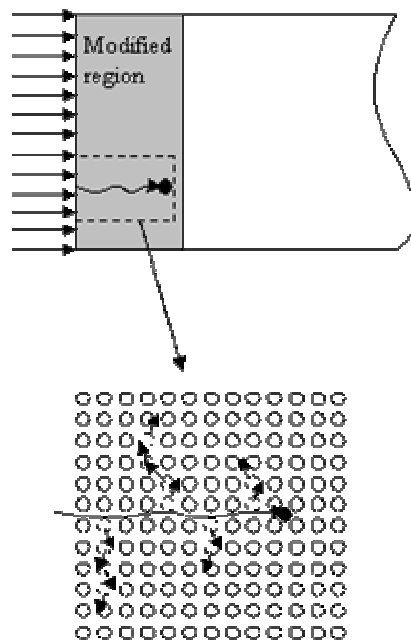
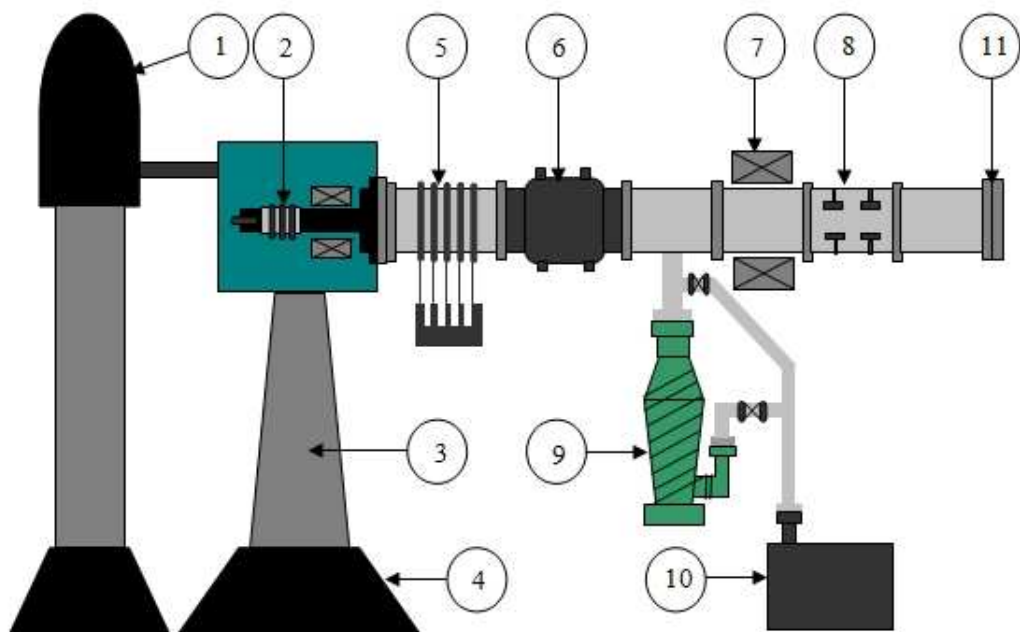


Figure 1: A schematic view of the path of an individual ion in ion implantation (Hirvonen and Sartwell, 1994).



- | | |
|----------------------------|----------------------|
| 1. High voltage source | 7. Magnetic analyzer |
| 2. Penning type ion source | 8. Beam sweeper |
| 3. Isolated column | 9. Diffusion pump |
| 4. Base | 10. Rotary pump |
| 5. Accelerator tube | 11. Target |
| 6. Quadrupole lenses | |

Figure 2: Schematic diagram of devices for ion implantation

Several researchers have utilized the ion implantation applications in the medical area, such as for orthopaedic prostheses that require high wear properties, excellent corrosion resistance and biocompatibility (Diaz et al., 2009; Jagielski et al., 2006; Huang et al., 2004).

The titanium alloy Ti-6Al-4V is widely in use for biomedical applications such as artificial hip and knee joints. Beneficial properties include improved ductility, tensile and fatigue strength, bone-matched modulus of elasticity and biocompatibility due to the native oxide layer (Torregrosa et al., 1995; Tsyganov et al., 2002). However, there are some concerns about the toxicity of Al and V wear debris in the human body that might negative side effects to the human body. For this reason, the use of cp titanium is a potential metal and safer to replace Ti-6Al-4V titanium alloy bearings. But, its wear properties still need to be improved (Darmawan et al., 2010).

It is generally known that ion implantation treatment can improve the mechanical wear properties of metals. In particular, nitrogen ion implantation is an excellent process to enhance the wear resistance of a wide range of ferrous materials and titanium-based alloys (Ikeda et al., 2002).

Improvement of the surface hardness and corrosion resistance are depended on the used of implantation parameters such as energy, dose or time. The dose, ϕ , is related to the beam current, I , by the following formula (Nastasi and Mayer, 2006):

$$\phi = \frac{It}{qiA} \tag{1}$$

Where,

t : implantation time

A : beam area

qi : the charge per ion

Beam current and implantation doses typically range from $1 \mu A - 30 mA$ and $10^{11} - 10^{19}$ atoms/cm²

In this study, the effects of the nitrogen ion doses to the surface hardness are then investigated. The surface hardness is measured by using Micro Vickers Hardness Tester.



Figure 3: Photograph of the device arrangement for ion implantation

Materials and Methods

The material used for this work is cp titanium. The chemical composition of cp titanium is as follows: N: 0.04%, C: 0.05%, H: 0.003%, Fe: 0.13%, O: 0.11%, Al: 0.49% S: 0.03, Ti: balance. The material has hardness number of 53.99 HV.

Regarding to ion implantation processes, cp titanium material is cut with the size of 1 cm x 1 cm x 0.3 cm. Specimens as many as three pieces created for this purpose. Then the material is grinded and polished using polycrystalline diamond until it is clean and shiny.

The ion implantation process is conducted by the ion implanter 200 kV/ 2mA. Nitrogen ion is implanted in target chamber of ICS-SP 1104. The energy of 100 keV and the current of 100 η A are applied. During ion implantation, the vacuum at the target chamber was maintained below 1×10^{-6} mBar. In this study, process durations are varied as 140 minutes, 280 minutes and 560 minutes.

Prior to hardness testing, a careful surface preparation (grinding and polishing) is conducted to ensure a well-defined indentation that may be accurately measured. This hardness test follows the standard ASTM E 384. The micro-hardness measurement works with indenter force as light as 10 gf (gram force), with indentation time in 15 seconds. The indenter is a square-based pyramidal-shaped diamond with a face angle of 136° . This indenter and its diagonals of impression are illustrated in Figure 4. After force removal, the impression diagonals are measured with a light microscope. It is assumed that the indentation does not undergo elastic recovery after force removal.

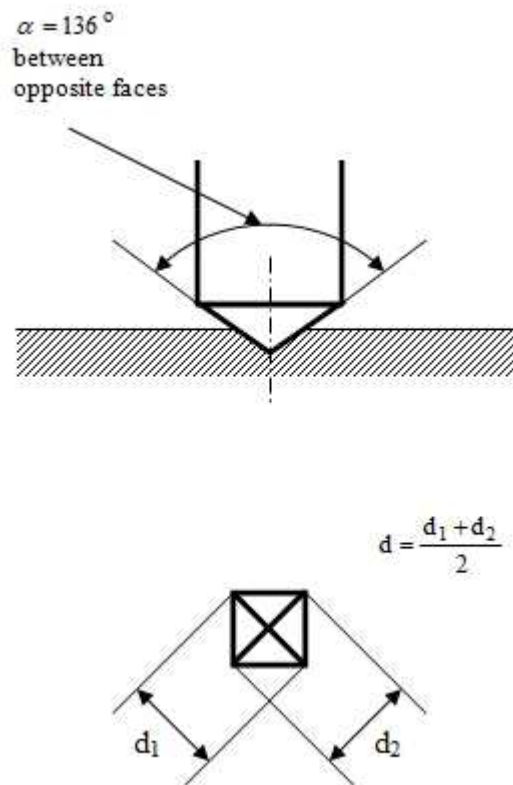


Figure 4: Vickers Hardness Test

The Vickers hardness number can be determined by the following equation:

$$HV = 1,854P / d^2 \tag{2}$$

where

P: the applied force (Kg),

d: mean diagonal of impression (mm).

Karl Frank GMBH Type 38505 micro hardness tester is used for measuring the hardness of the specimen. This micro hardness tester can be seen in Figure 5.

Results and Discussions

The results are analyzed and plotted to see the effect of ion implantation process doses to the material hardness.

Doses Calculation for Ion Implantation: Using Eq.1, the dose required for ion implantation is calculated for each duration process. For example, the dose calculation for beam current, $I = 100 \mu A$, implantation time, $t = 140 \text{ minutes} = 8400 \text{ second}$, beam area, $A = 1 \text{ cm}^2$, the charge per ion, $qi = 1.6 \times 10^{-19} \text{ coulomb}$ is as follows:

$$\phi = \frac{It}{qiA}$$

$$\phi = \frac{100 \times 8400}{1.6 \times 10^{-19} \times 1}$$

$$\phi = 8.4 \times 10^{14} \text{ ions/cm}^2$$

Similarly, the dose required is calculated, the result can be seen in table 1.



Fig. 5: Karl Frank GMBH Type 38505 Buehler Micro hardness tester

Table 1 Result of dose calculation for various duration

Duration [minutes]	Dose [ions/cm ²]
140	8.4x10 ¹⁴
280	16.8x10 ¹⁴
560	33.6x10 ¹⁴

Surface hardness calculation: After the specimens are ion implantation processed, hardness testing is conducted on the surface of the specimens. Using Eq.2, the surface hardness is calculated for each duration process. Then the results can be seen in table 2.

Table 2 Surface Hardness due to ion implantation process

Duration [minutes]	Dose [ions/cm ²]	Hv
140	8.4x10 ¹⁴	88.97
280	16.8x10 ¹⁴	125.51
560	33.6x10 ¹⁴	130.2

The Effect of Ion Implantation Process Doses to the Material Hardness: The hardness values for ion implantation processes for doses of 8.4x10¹⁴ ions/cm², 16.8x10¹⁴ ions/cm², and 33.6x10¹⁴ ions/cm² are 88.97 HV,

125.51 HV, and 130.2 HV, respectively. Compared to the hardness of the raw material, these processes have increased the hardness values by 64.8 %, 132.5 %, and 141.2 % respectively.

There is a significant increased in hardness value when the dose is increased from 8.4×10^{14} ions/cm² to 16.8×10^{14} ions/cm². The hardness can be improved as high as 41.07%.

The hardness improvement, however does not show a linear behavior when the dose is increased. When the dose is increased to 33.6×10^{14} ions/cm², the hardness value is increased only 3.74%. The hardness improvement is not significant when it is compared with that of dose increasing from 8.4×10^{14} ions/cm² to 16.8×10^{14} ions/cm². The hardness values are illustrated in Figure 6.

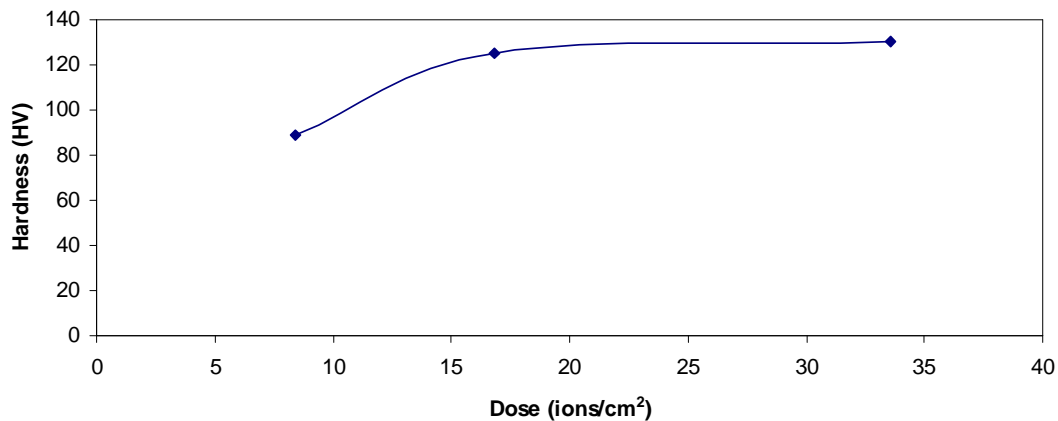


Figure 6: The hardness values in the surface of specimen which is processed ion implantation.

The results of ion implantation test showed the longer the duration the higher the value of the resulting hardness. This is because the longer the process duration the greater the number of nitrogen ions diffuse into the surface of titanium (see again table 1) so the greater the number of TiN compound is formed on the surface.

Conclusions

In this research, the surface hardness of cp titanium is modified and improved by using ion implantation process. The effects of such processes to hardness value can be concluded as the followings:

1. The ion implantation of cp titanium can significantly increase the hardness on the surface.
2. Compared to the hardness of the raw material, these processes have increased the hardness values by 64.8 %, 132.5 %, and 141.2 % for the doses of 8.4×10^{14} ions/cm², 16.8×10^{14} ions/cm², and 33.6×10^{14} ions/cm² respectively
3. The hardness can be improved as high as 41.07% when the dose is increased from 8.4×10^{14} ions/cm² to 16.8×10^{14} ions/cm². However there is no a significant increased in hardness value when the dose is increased from 16.8×10^{14} ions/cm² to 33.6×10^{14} ions/cm².

Acknowledgement

The authors gratefully acknowledge financial support from Universiti Tun Hussein Onn Malaysia under Fund Scheme GIS Vot 0809. The authors also would like to thank Accelerator Application Group of BATAN-Yogyakarta Indonesia for allowing ion implantation processes be conducted in its laboratory; Material Laboratory of Universitas Gajah Mada Indonesia for micro Vickers hardness test and Mechanical Engineering Laboratory of Universitas Muhammadiyah Surakarta for all specimens preparation.

References:

- Darmawan, A. S., Siswanto, A. S. and Samekto, H., (2010), "Effect of Femoral Head Size to Contact Stress at Pure Titanium Femoral Ball Head Outer Surface of Hip Joint Implant", *Proceeding of National Conference on Advanced Manufacturing and Materials, Universiti Tun Hussein Onn Malaysia, Malaysia*, pp. 18
- Díaz, C., Lutz, J., Mändl, S., García, J.A., Martínez, R., and Rodríguez, R. J., (2009), "Improved bio-tribology of biomedical alloys by ion implantation techniques", *Nuclear Instruments and Methods in Physics Research*, Vol. B 267, pp. 1630–1633
- Hirvonen, J. K. and Sartwell, B. D., (1994), "Ion Implantation", *ASM Handbook*, Vol. 5, pp. 1680-1690

- Huang, N., Yang, P., Leng, Y. X., Wang, J., Sun, H., Chen, J. Y., and Wan, G. J., (2004), “Surface modification of biomaterials by plasma immersion ion implantation”, *Surface & Coatings Technology*, Vol. 186, pp. 218–226
- Ikeda, D., Ogawa, M., Hara, Y., Nishimura, Y., Odusanya, O., Azuma, K., Matsuda, S., Yatsuzuka, M., and Murakami, A., (2002), “Effect of nitrogen plasma-based ion implantation on joint prosthetic material”, *Surface and Coatings Technology*, Vol. 156, pp. 301–305
- Jagielski, J., Piatkowska, A., Aubert, P., Thomé, L., Turos, A., and Kader, A. A., (2006), “Ion implantation for surface modification of biomaterials”, *Surface & Coatings Technology*, Vol. 200, pp. 6355–6361
- Nastasi, M., and Mayer, J. W., (2006), “Ion Implantation and Synthesis of Materials”, Springer, Berlin, German,
- Torregrosa, F., Barrallier, L., and Roux, L., (1995), “Phase analysis, microhardness and tribological behaviour of Ti-6Al-4V after ion implantation of nitrogen in connection with its application for hip-joint prosthesis”, *Thin Solid Films*, Vol. 266, pp. 245-253
- Tsyganov, I., Wieser, E., Matz, W., Reuther, H., and Richter, E., (2002), “ Modification of the Ti-6Al-4V alloy by ion implantation of calcium and/or phosphorus”, *Surface and Coatings Technology*, Vol. 158 –159, pp. 318–323